

Linearization of FAST with AeroDyn & HydroDyn



**NREL Wind Turbine
Modeling Workshop**

March 2, 2012

NREL – Golden, CO

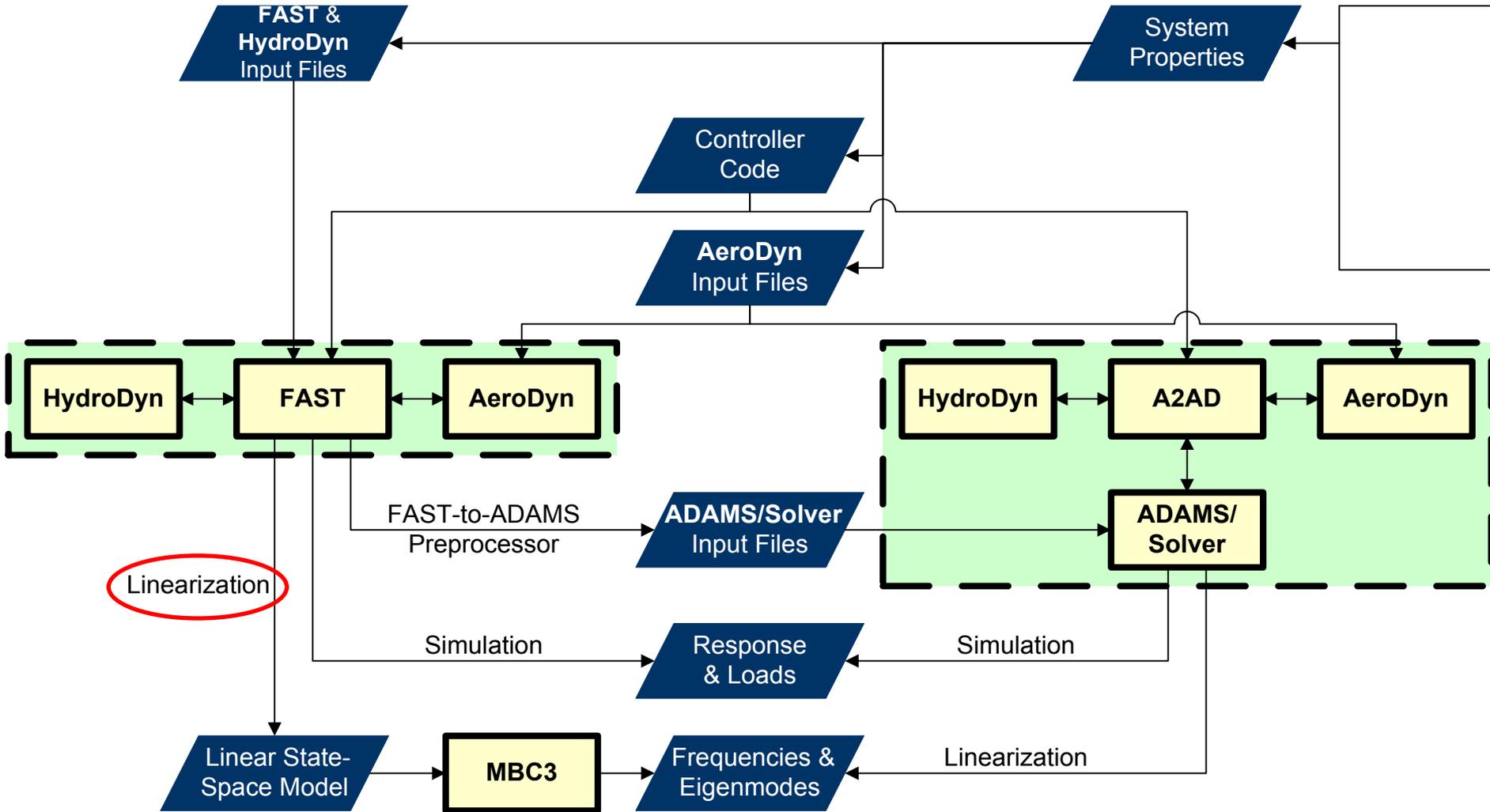
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Outline

- Modes of Operation
- Background
- Calculating Operating Points
- Model Linearization:
 - 2nd-Order Model
 - 1st-Order Model
 - Numerics
- Example – Campbell Diagram for OC3-Hywind
- Current & Planned Work & Future Opportunities

Linearization

Modes of Operation



Linearization

Background

- Creates linear representation of nonlinear system model
- Applications:
 - Full-system modal analysis:
 - Frequencies
 - Damping
 - Mode shapes
 - Stationary or operational
 - Controls design:
 - Develop state-space representation of wind turbine “plant”
 - Includes control inputs, wind disturbances, & output
 - Stability analysis
- Linear model is only valid in the local vicinity of an operating point (OP):
 - Requires that one select or compute an OP before linearization
- When rotor is spinning, the linear system is periodic:
 - Azimuth-averaging averages-out the periodic effects
 - Multi-blade coordinate (MBC) expresses cumulative effect of blade dynamics in the fixed frame

Linearization

Calculating Operating Points

- Operating point choices:
 - Initial condition (user-selected) (watch out for nonstationary OP!)
 - Static equilibrium (parked or idling)
 - Periodic steady-state equilibrium (operational):
 - No trim: All controls fixed (fixed speed)
 - Trim: One control input varied to achieve desired rotor speed:
 - Nacelle yaw
 - Generator torque
 - Blade pitch
- Equilibrium solutions found through time-domain simulation:
 - Solution found within user-selected displacement & velocity tolerances
 - Solution can be sped up with optional compile-time feature to artificially increase system damping
 - Optional trim calculation is automated with a proportional feedback control law on rotor-speed error

Linearization

Model Linearization – 2nd-Order Model

Nonlinear EoM:

$$M(\underline{q}, \underline{u}, t) \ddot{\underline{q}} + \underline{f}(\underline{q}, \dot{\underline{q}}, \underline{u}, \underline{u}_d, t) = \underline{0}$$

Nonlinear Outputs:

$$\underline{OutData} = \underline{Y}(\underline{q}, \dot{\underline{q}}, \underline{u}, \underline{u}_d, t) = \underline{Y}_r(\underline{q}, \underline{u}, t) \dot{\underline{q}} + \underline{Y}_t(\underline{q}, \dot{\underline{q}}, \underline{u}, \underline{u}_d, t)$$

Perturbation of system variables:

$$\underline{q} = \underline{q}|_{op} + \underline{\Delta q} \quad \dot{\underline{q}} = \dot{\underline{q}}|_{op} + \underline{\Delta \dot{q}} \quad \underline{u} = \underline{u}|_{op} + \underline{\Delta u} \quad \underline{u}_d = \underline{u}_d|_{op} + \underline{\Delta u}_d \quad \rightarrow \quad \ddot{\underline{q}} = \ddot{\underline{q}}|_{op} + \underline{\Delta \ddot{q}} \quad \underline{Y} = \underline{Y}|_{op} + \underline{\Delta Y}$$

Linear EoM:

$$M \underline{\Delta \ddot{q}} + C \underline{\Delta \dot{q}} + K \underline{\Delta q} = F \underline{\Delta u} + F_d \underline{\Delta u}_d$$

$$M = M|_{op}$$

$$C = \left. \frac{\partial \underline{f}}{\partial \dot{\underline{q}}} \right|_{op}$$

$$K = \left. \left[\frac{\partial M}{\partial \underline{q}} \ddot{\underline{q}} + \frac{\partial \underline{f}}{\partial \underline{q}} \right] \right|_{op}$$

$$F_d = - \left. \frac{\partial \underline{f}}{\partial \underline{u}_d} \right|_{op}$$

$$F = - \left. \left[\frac{\partial M}{\partial \underline{u}} \ddot{\underline{q}} + \frac{\partial \underline{f}}{\partial \underline{u}} \right] \right|_{op}$$

Linear Outputs:

$$\underline{\Delta Y} = \underline{VelC} \underline{\Delta \dot{q}} + \underline{Dsp} \underline{\Delta q} + \underline{D} \underline{\Delta u} + \underline{D}_d \underline{\Delta u}_d$$

$$\underline{VelC} = \left. \frac{\partial \underline{Y}}{\partial \dot{\underline{q}}} \right|_{op} = \left. \left[-\underline{Y}_r M^{-1} C + \frac{\partial \underline{Y}_t}{\partial \dot{\underline{q}}} \right] \right|_{op}$$

$$\underline{DspC} = \left. \frac{\partial \underline{Y}}{\partial \underline{q}} \right|_{op} = \left. \left[\frac{\partial \underline{Y}_r}{\partial \underline{q}} \ddot{\underline{q}} - \underline{Y}_r M^{-1} K + \frac{\partial \underline{Y}_t}{\partial \underline{q}} \right] \right|_{op}$$

$$\underline{D} = \left. \frac{\partial \underline{Y}}{\partial \underline{u}} \right|_{op} = \left. \left[\frac{\partial \underline{Y}_r}{\partial \underline{u}} \ddot{\underline{q}} + \underline{Y}_r M^{-1} F + \frac{\partial \underline{Y}_t}{\partial \underline{u}} \right] \right|_{op}$$

$$\underline{D}_d = \left. \frac{\partial \underline{Y}}{\partial \underline{u}_d} \right|_{op} = \left. \left[\underline{Y}_r M^{-1} F_d + \frac{\partial \underline{Y}_t}{\partial \underline{u}_d} \right] \right|_{op}$$

(matrix sizes determined by enabled DOFs)

Linearization

Model Linearization – 1st-Order Model

Conversion From 2nd Order to 1st Order:

$$\underline{x} = \begin{Bmatrix} \underline{\Delta q} \\ \underline{\Delta \dot{q}} \end{Bmatrix} \quad \underline{\dot{x}} = \begin{Bmatrix} \underline{\Delta \dot{q}} \\ \underline{\Delta \ddot{q}} \end{Bmatrix} \quad \underline{y} = \underline{\Delta Y}$$

Linear EoM & Outputs:

$$\underline{\dot{x}} = A\underline{x} + B\underline{\Delta u} + B_d \underline{\Delta u}_d$$

$$\underline{y} = C\underline{x} + D\underline{\Delta u} + D_d \underline{\Delta u}_d$$

$$A = \begin{bmatrix} 0 & I \\ -M^{-1}K & -M^{-1}C \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ M^{-1}F \end{bmatrix} \quad B_d = \begin{bmatrix} 0 \\ M^{-1}F_d \end{bmatrix} \quad C = [D_{sp}C \quad VelC]$$

Linearization

Model Linearization – Numerics

- Linearization done numerically with central-difference method:
 - Perturbations made about OP
 - Perturbations are hard-coded:
 - Default perturbation: 2°
 - Can be changed at compile time

$$-M^{-1}C = \frac{\ddot{q}(\dot{q}|_{op} + \Delta\dot{q}) - \ddot{q}(\dot{q}|_{op} - \Delta\dot{q})}{2\Delta\dot{q}}$$

$$VelC = \frac{Y(\dot{q}|_{op} + \Delta\dot{q}) - Y(\dot{q}|_{op} - \Delta\dot{q})}{2\Delta\dot{q}}$$

$$-M^{-1}K = \frac{\ddot{q}(q|_{op} + \Delta q) - \ddot{q}(q|_{op} - \Delta q)}{2\Delta q}$$

$$DspC = \frac{Y(q|_{op} + \Delta q) - Y(q|_{op} - \Delta q)}{2\Delta q}$$

$$M^{-1}F = \frac{\ddot{q}(u|_{op} + \Delta u) - \ddot{q}(u|_{op} - \Delta u)}{2\Delta u}$$

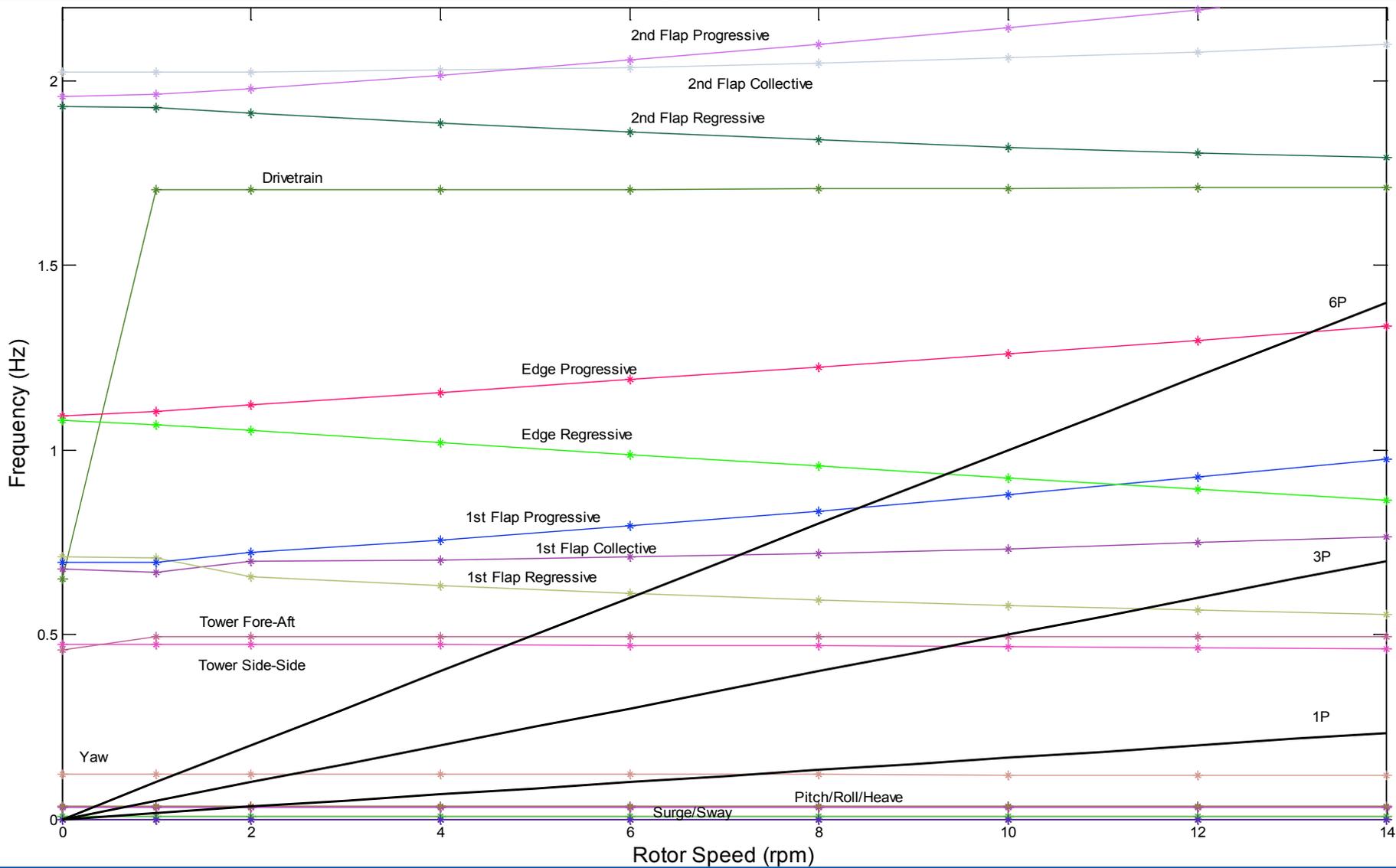
$$D = \frac{Y(u|_{op} + \Delta u) - Y(u|_{op} - \Delta u)}{2\Delta u}$$

$$M^{-1}F_d = \frac{\ddot{q}(u_d|_{op} + \Delta u_d) - \ddot{q}(u_d|_{op} - \Delta u_d)}{2\Delta u_d}$$

$$D_d = \frac{Y(u_d|_{op} + \Delta u_d) - Y(u_d|_{op} - \Delta u_d)}{2\Delta u_d}$$

Linearization

Example – Campbell Diagram for OC3-Hywind



Current & Planned Work & Future Opportunities

- Current & Planned Work:
 - Minor improvements
- Future Opportunities:
 - Include states, inputs, & outputs from all modules during linearization:
 - Aerodynamics
 - Hydrodynamics
 - Controls

Questions?



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