

Monopile as part of aeroelastic
code BHawC

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Monopile as part of aeroelastic code

Jørgen Thirstrup Petersen & Rune Rubak

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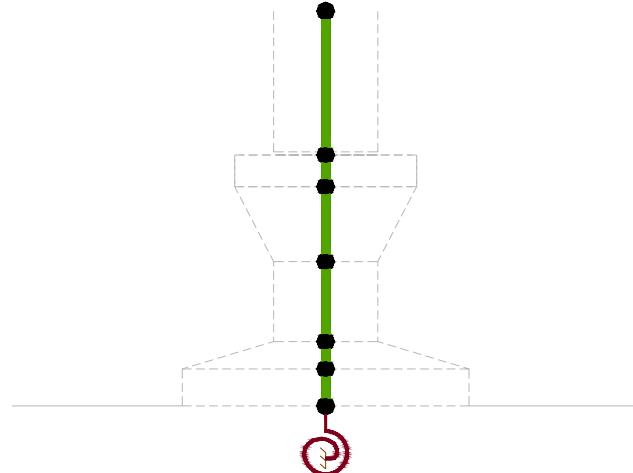
PRESENTATION OUTLINE

- SWP offshore aeroelastic model techniques
- BHawC non-linear aeroelastic code
- Integrated monopile
- Case study

Offshore aeroelastic model techniques

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- Gravity based concrete structure
 - Shallow water
 - Stiff structure
 - High soil strength
 - Preloaded soil
- Model method
 - Timoschenko beam elements
 - Translational and rotational soil spring



Offshore aeroelastic model techniques

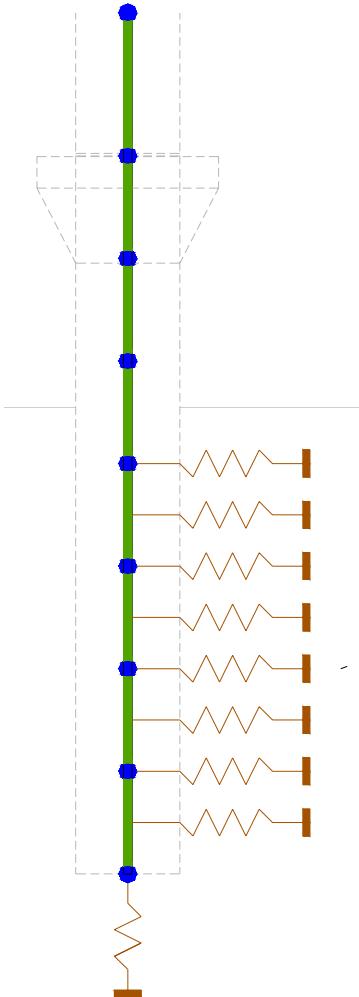
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- Monopile foundation
 - Shallow and deeper water
 - Flexible structure
 - Soil strength variation
 - Unloaded soil
- Model method 1
 - Part of monopile with beam elements
 - Equivalent fixation point

Offshore aeroelastic model techniques

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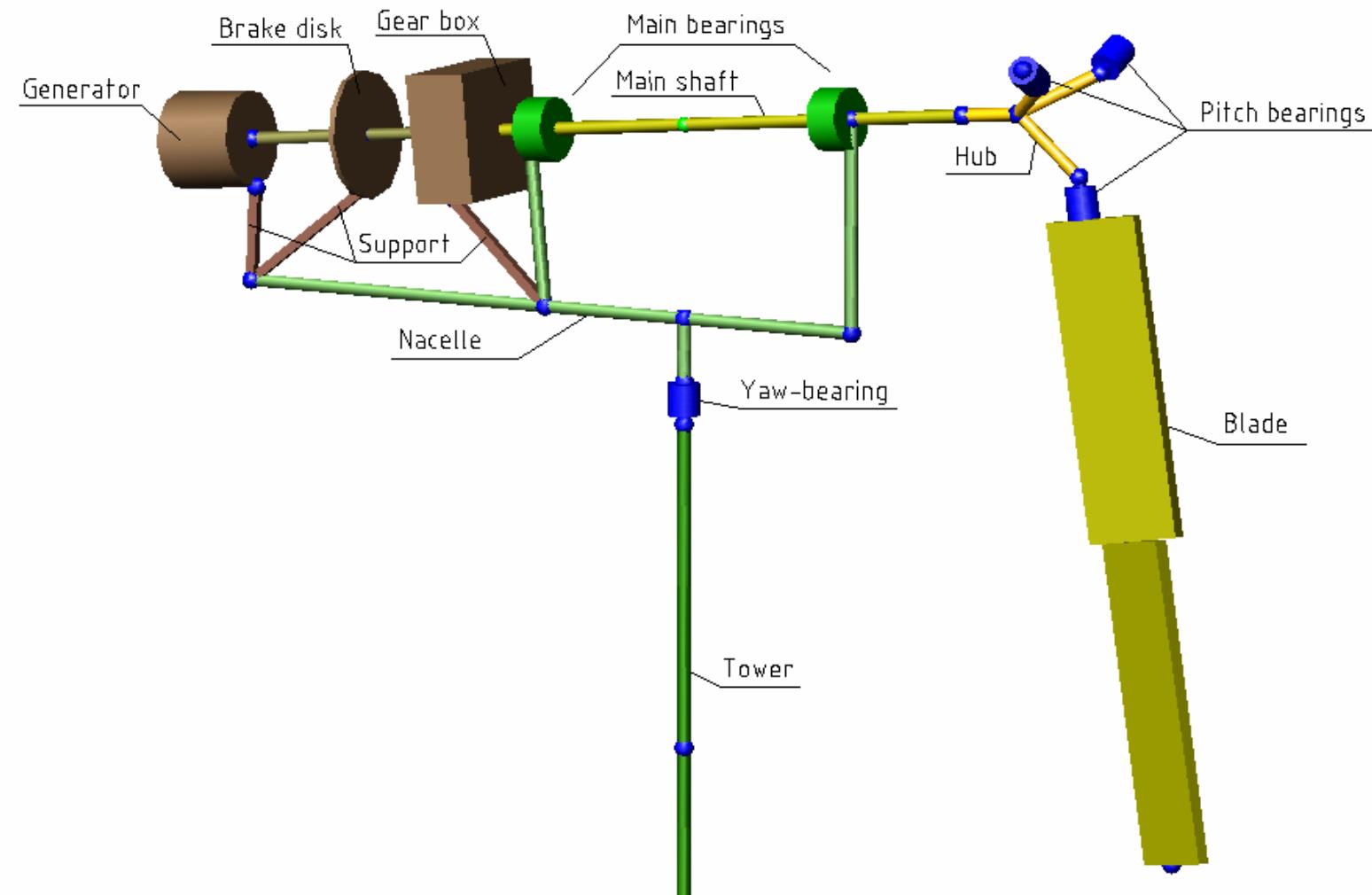
- Monopile foundation
 - Shallow and deeper water
 - Flexible structure
 - Soil strength variation
 - Unloaded soil
- Model method 1
 - Part of monopile with beam elements
 - Equivalent fixation point
- Model method 2
 - Full monopile with beam elements
 - Non-linear soil springs



- **BHawC: BONUS ENERGY Horizontal axis wind turbine Code**
 - Jørgen Thirstrup Petersen
 - Rune Rubak
- Development milestones
 - 02 / 2003: Static non-linear simulation
 - 10 / 2003: Dynamic non-linear simulation
 - 08 / 2004: Comparison with HawC 2.3MW CombiStall® turbine
 - 04 / 2005: IEC design load calculation
 - 08 / 2005: Basic load verification on 2 turbines
 - ?? / ?????: Detailed load verification
- Performance
 - Calculates with 0.2·realtime on PC

BHawC – Structural model turbine

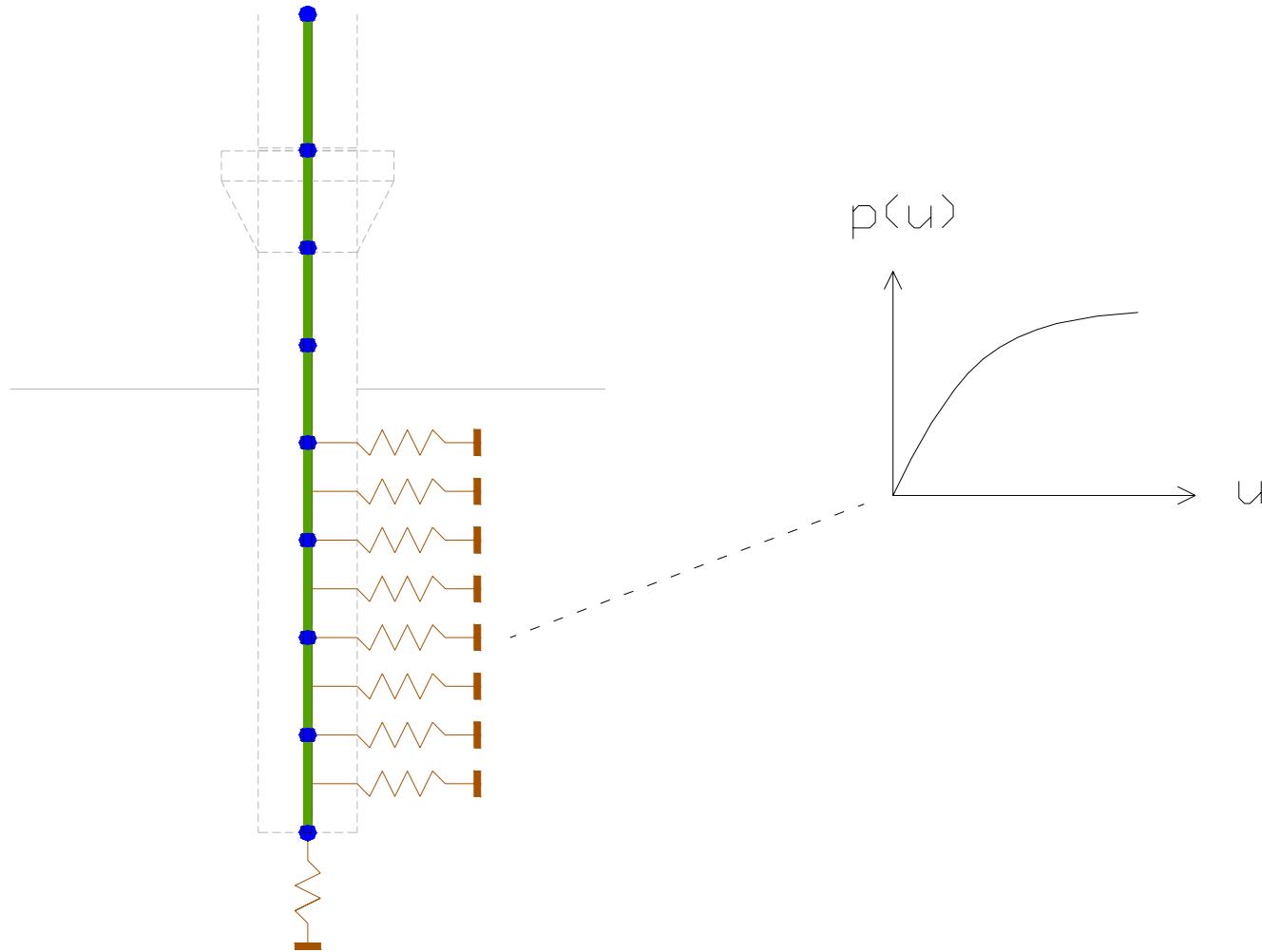
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BHawC – Integrated monopile model

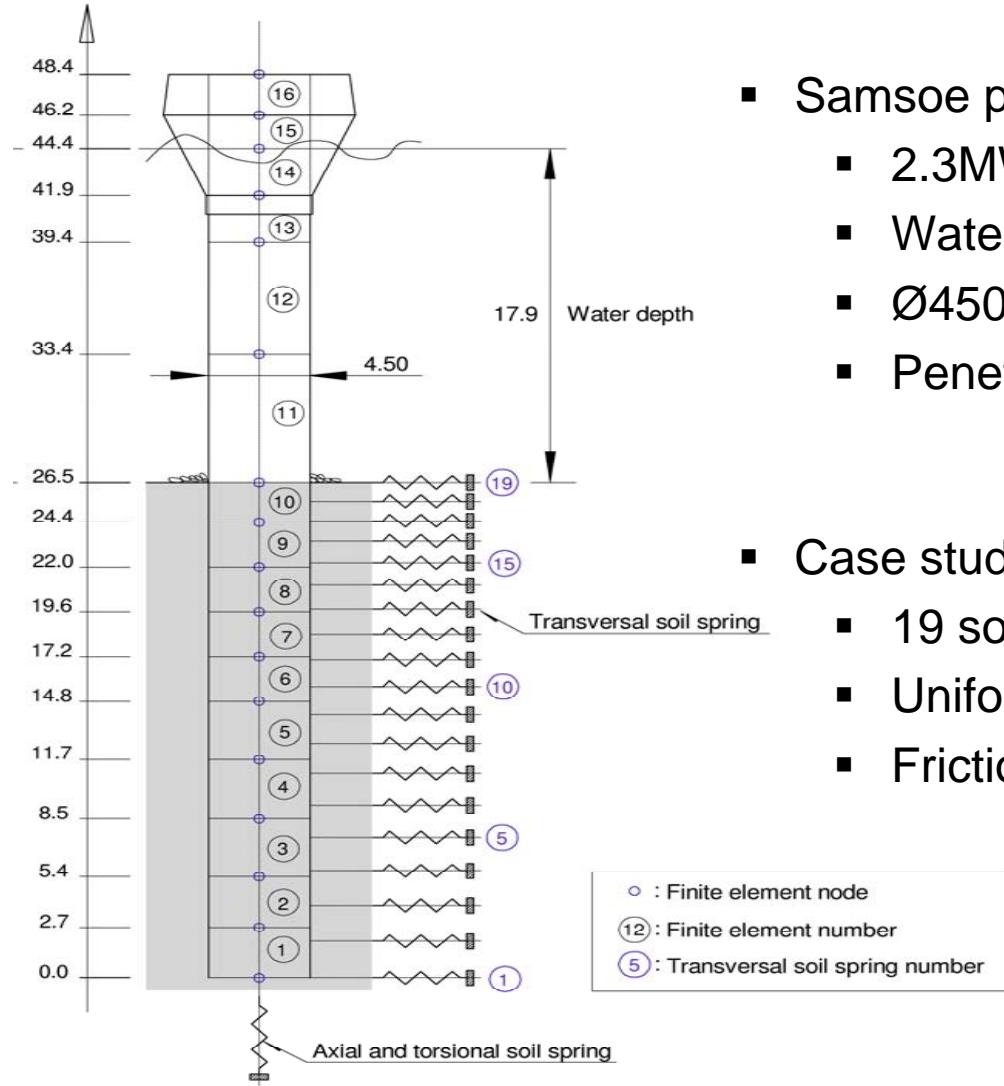
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- Aerodynamic blade loads
 - BEM
 - Yaw correction
 - Tower shadow
 - Dynamic inflow
 - Dynamic stall model
- Nacelle and tower aerodynamic loads
- Wave loads
- Gravity loads

Case study - Description

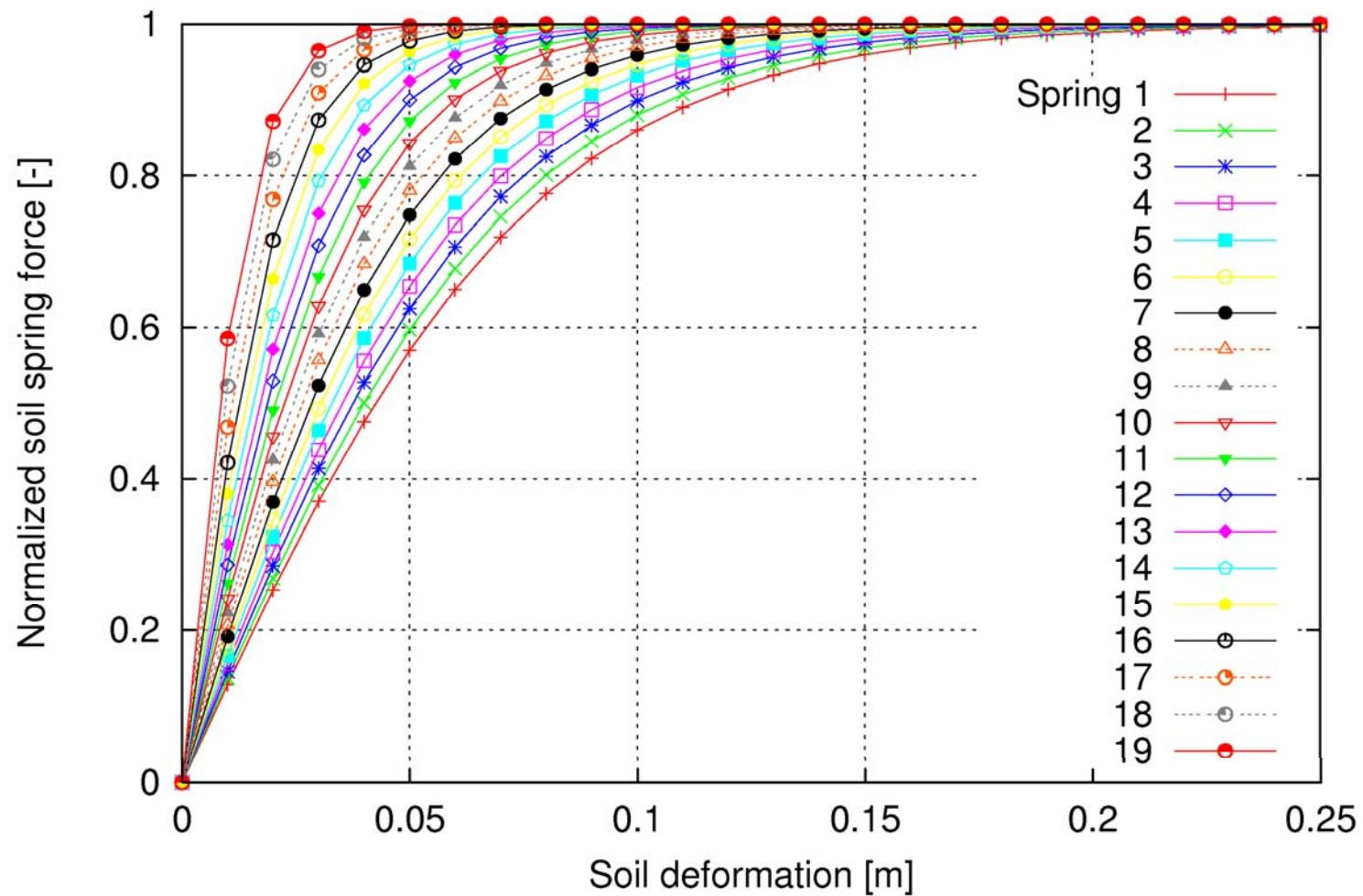
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- Samsoe project basis
 - 2.3MW turbine - CombiStall® regulation
 - Water depth 17.9 m
 - Ø4500 monopile
 - Penetration depth 26.5 m
- Case study
 - 19 soil springs
 - Uniform sand assumed
 - Friction angle 24°, 30° and 36°

Case study – Description

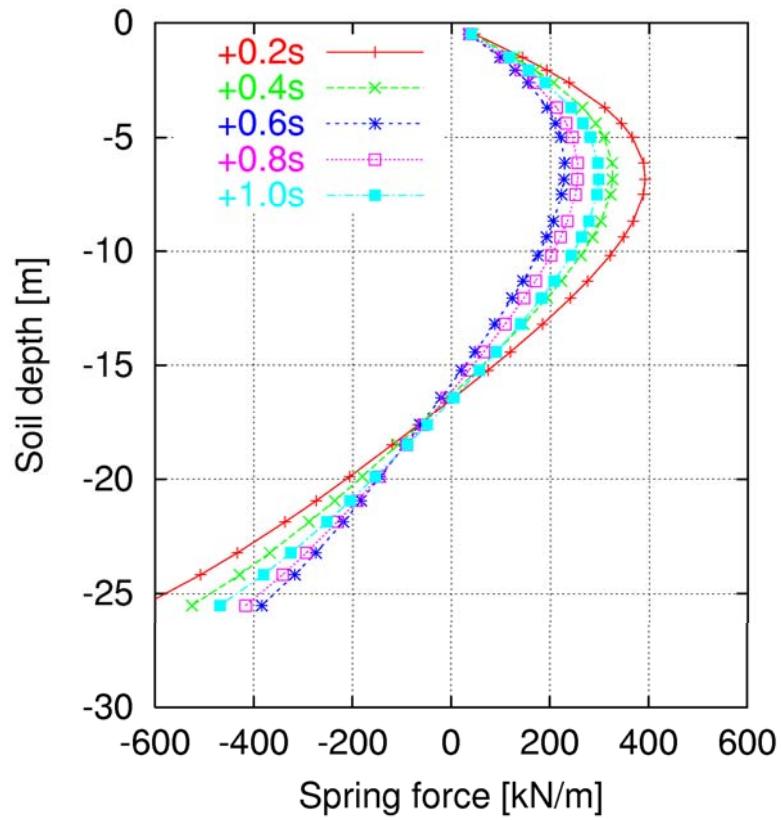
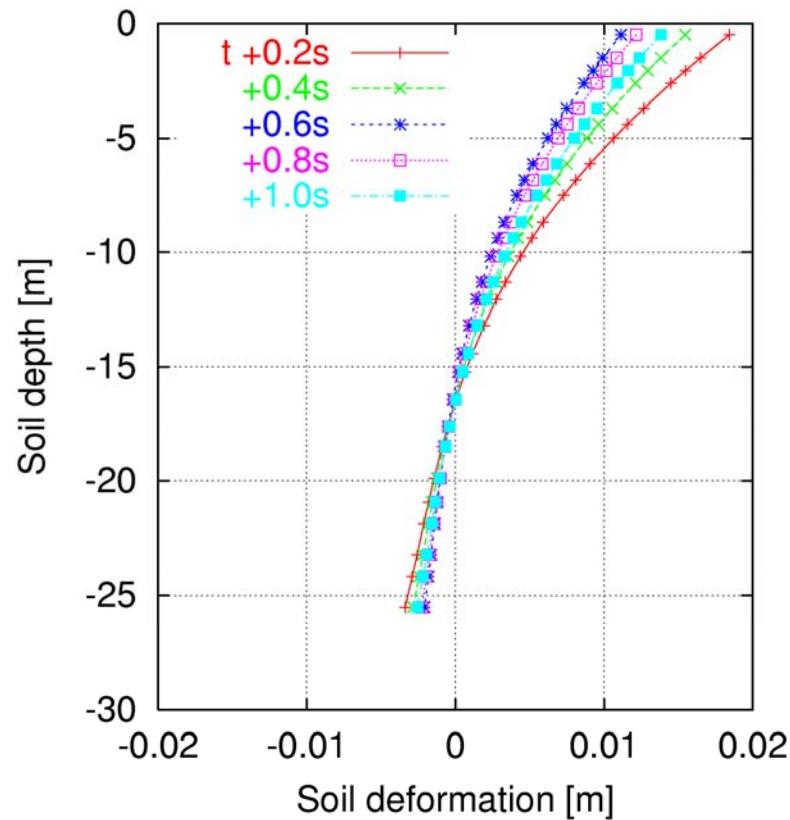
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Case study – Results

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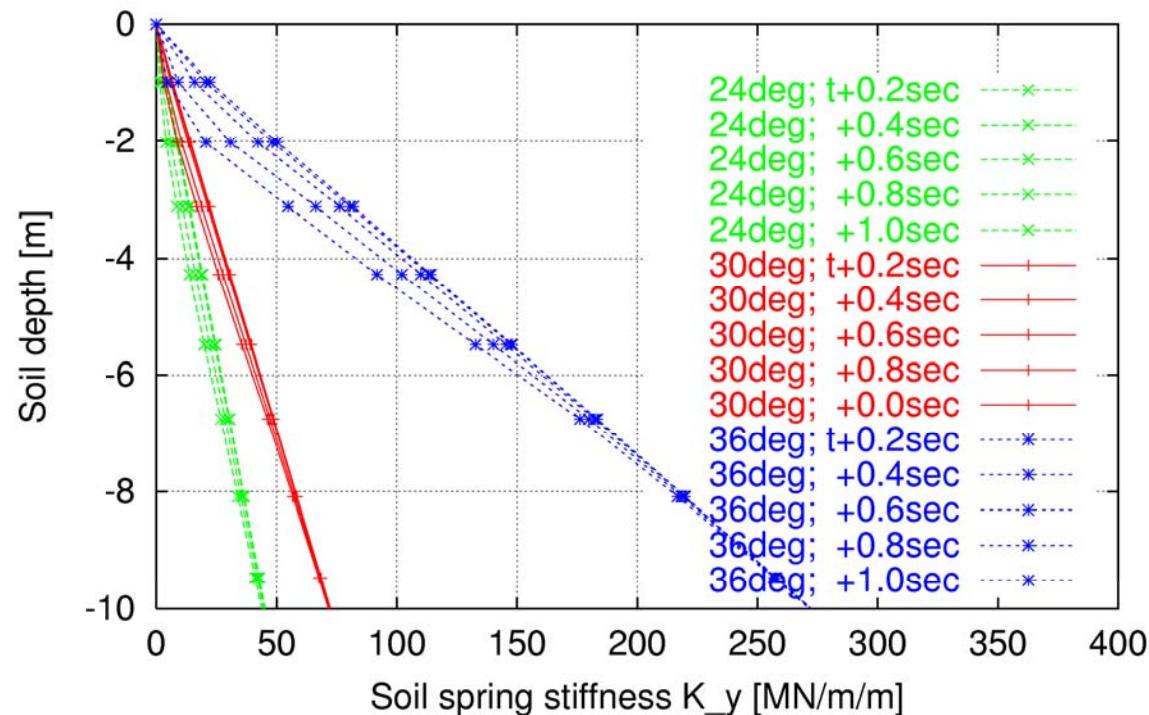
- Snapshots of longitudinal deformation and soil spring force



Case study – Results

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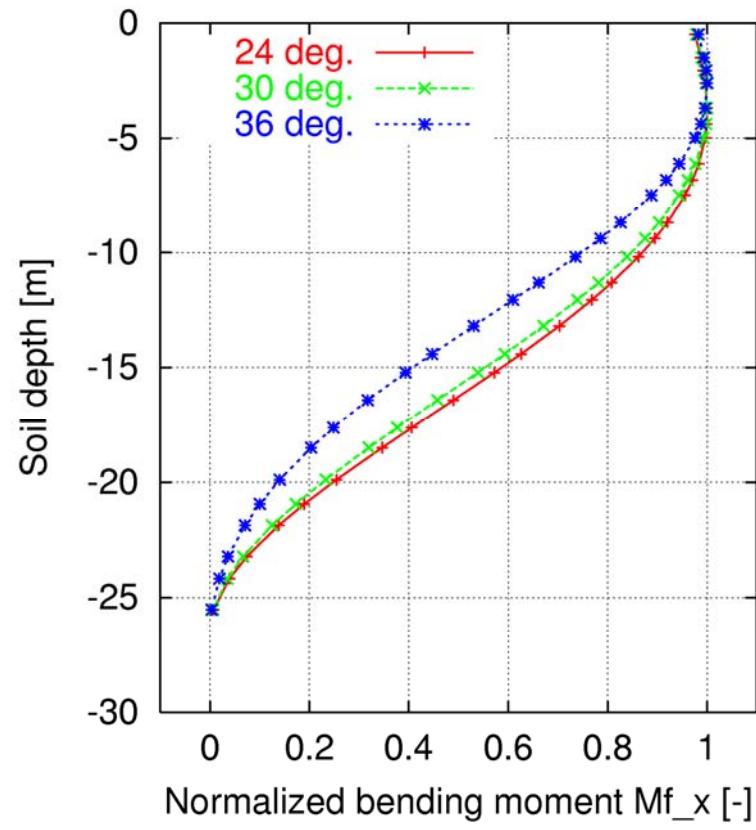
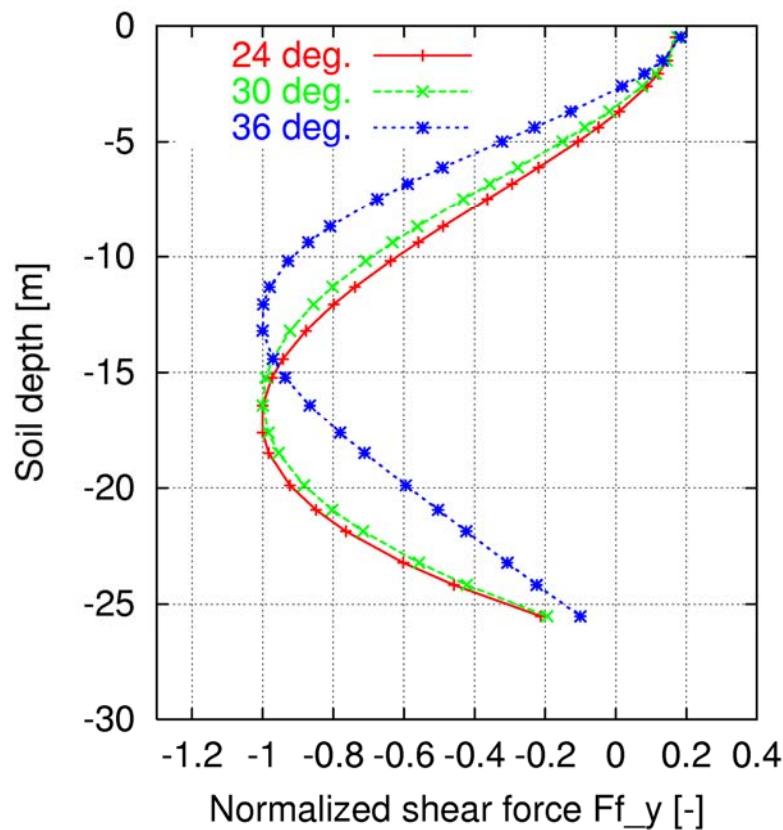
- Snapshots of soil spring stiffness



Case study – Results

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- Shear force and bending moment



Case study - Results

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- Main changes in natural frequencies

Mode shape	Friction angle		
	24°	30°	36°
1st tower	-3%	Baseline	+6%
2nd rotor tilt	-6%	Baseline	+13%
2nd rotor yaw	-7%	Baseline	+13%

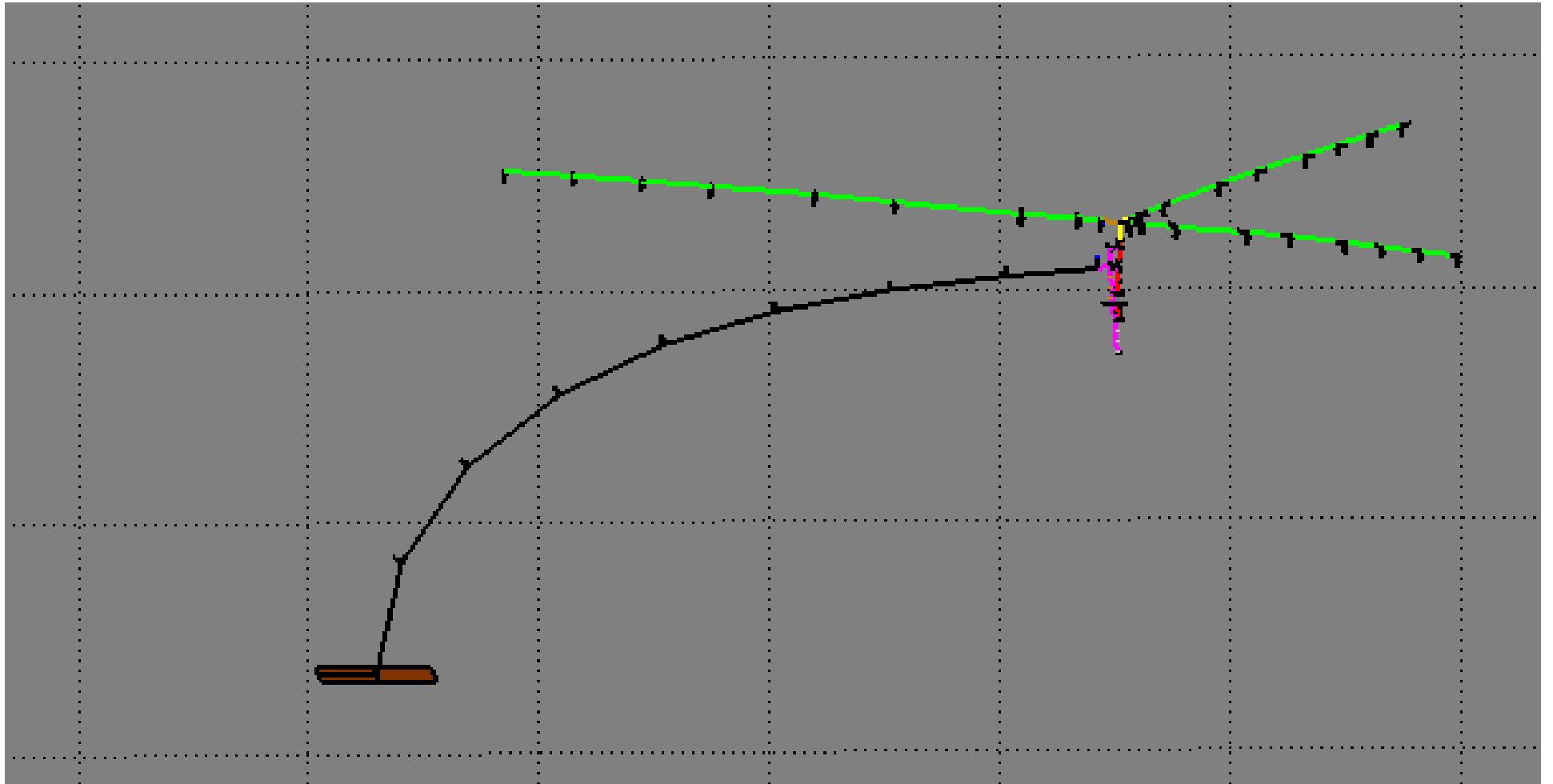
Case study – Fatigue loads

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- Impact on lifetime fatigue loads
 - Based on 5, 10, 15, 20 and 25 m/s

Bending moment	Friction angle		
	24°	30°	36°
Mudline	+24%	Baseline	-19%
Tower base	+30%	Baseline	-24%
Shaft-hub flange	-1%	Baseline	+5%
Blade flapwise	+1%	Baseline	+3%
Blade edgewise	+0%	Baseline	+40%

- Aeroelastic code BHawC
 - Non-linear FEM model of turbine
 - Integrated monopile model
- Improvements with monopile model
 - Cross section forces available below mudline
 - Mode shapes and natural frequencies
 - Fatigue load estimation improved
- Further developments
 - Soil stiffness and damping models
 - Effect on extreme loads
 - Load verification



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